Figure 4.1 - Alternative Flow Dispersal Trench


## NOTES:

1. This trench shall be constructed to prevent point discharge and /or erosion.
2. Trenches may be placed no closer than 50 feet to one another (100 feet along flowline).
3. Trench and grade board must be level. Align to follow contours of site.
4. Support post spacing as required by soil conditions to ensure grade board remains level.
*15\% max for flow control/water quality treatment in rural areas

SECTION A-A
NTS



## A. Metal and Concrete Pipe



## B. Pipe - Installation

## Rigid Pipe NOTES:

1. Pipe compaction limits shown on this plan are for pipe construction in an embankment. For pipe construction in a trench, the horizontal limits of the pipe compaction zone shall be the walls of the trench.
2. All steel and aluminum pipe and pipe-arches shall be installed in accordance with design A.
3. Concrete pipe with elliptical reinforcement shall be installed in accordance with design A.
4. Concrete pipe, plain or with circular reinforcement, shall be installed with design $A$.
5. O.D. is equal to the outside diameter of a pipe or the outside span of pipe-arch. The dimensions shown as O.D. with 3' maximum shall be O.D. until O.D. equals 3'; at which point 3 ' shall be used.

* 1 '-0" for diameters 12 " through 42" and spans through $50 "$. $2^{\prime}-0^{\prime \prime}$ for diameters greater than $42^{\prime \prime}$ and spans greater than 50 ".



## Bedding for Flexible Pipe

## Flexible Pipe NOTES:

1. Provide uniform support under barrels.
2. Hand tamp under haunches.
3. Compact bedding material to $95 \%$ max. density; directly over pipe, hand tamp only.
4. See "Excavation and Preparation of Trench" in sanitary sewers section of the standard WSDOT/APWA specifications for trench width "W" and trenching options. The pipe zone will be the actual trench width.
The minimum concrete width shall be $1{ }_{2}^{1}$ I.D. $+18{ }^{\prime \prime}$.
5. Trench backfill shall conform to "Backfilling Sewer Trenches" in the sanitary sewers section of the WSDOT/APWA standard specifications, except that rocks or lumps larger than 1" per foot of pipe diameter shall not be used in the backfill material.
6. See "Bedding Material for Flexible Pipe" in aggregates section of the WSDOT/APWA standard specifications for the material specifications.

Backfill material placed in 0.5 ' loose layers and compacted to $95 \%$ maximum density.
Method B or C compaction (WSDOT/APWA) standard specifications.)

| Pipe | Size | Min. dist. between barrels |
| :---: | :---: | :---: |
| circular pipe conc., LCPE, CMP (diameter) | $12^{\prime \prime}$ to 24" | 12" |
|  | 30" to 96" | diam. / 2 |
|  | 102" to 180" | 48" |
| pipe - arch metal only (span) | 18 " to $36 "$ | 12" |
|  | $43^{\prime \prime}$ to 142" | span / 3 |
|  | 148" to 199" | 48" |

Figure 4.3 - Pipe Anchor Detail


Figure 4.4 - Corrugated Metal Pipe Coupling and/or General Pipe Anchor Assembly


Smooth Coupling Band for Smooth Pipe


Plate Detail

$\angle$ flatten to point

> Anchor Assembly Corrugated Metal Pipe

NOTE:

1. The smooth coupling band shall be used in combination with concrete pipe.
2. Concrete pipe without ball and spigot shall not be installed on grades in excess of $20 \%$.
3. The first anchor shall be installed on the first section of the lower end of the pipe and remaining anchors evenly spaced throughout the installation.
4. If the pipe being installed has a manhole or catch basin on the lower end of the pipe, the first pipe anchor may be eliminated.
5. When CMP is used, the anchors may be attached to the coupling bands used to join the pipe as long as the specified spacing is not exceeded.
6. All pipe anchors shall be securely installed before backfilling around the pipe.

Figure 4.5 - Pipe Culvert Discharge Protection


Figure 4.6 - Debris Barrier (Off Road Right-of-Way)

## NOTE:

1. This debris barrier is for use outside roadways on pipes
$36 "$ dia. and smaller. See Figure 4.2.1.E for debris barriers on pipes projecting from driveway or roadway sideslopes.
2. All steel parts must be galvanized and asphalt coated (treatment 1 or better).
3. LCPE pipe requires bolts to secure debris barrier to pipe.

$\frac{\text { PLAN }}{\text { NTS }}$


ISOMETRIC NTS


Figure 4.7 - Debris Barrier (In Road Right-of-Way)

## NOTES:

1. CMP or LCPE pipe end-section shown; for concrete pipe beveled end section, see KCRS drawing No. 2-001.
2. All steel parts must be galvanized and asphalt coated (treatment 1 or better).


Figure 4.8 - Flow Dispersal Trench

*15\% max for flow control/water quality treatment in rural areas.

## SECTION A-A

NTS


## NOTES:

1. This trench shall be constructed to prevent point discharge and/or erosion.
2. Trenches may be placed no closer than 50 feet to one another (100 feet along flowline).
3. Trench and grade board must be level. Align to follow contours of site.
4. Support post spacing as required by soil conditions to ensure grade board remains level.

Figure 4.9 - Gabion Mattress Dissipater Detail


Figure 4.10 - Tee Type Energy Dissipater


Figure 4.11 - Inlet / Outlet Control Conditions


Inlet Control - Submerged Inlet


Inlet Control - Unsubmerged Inlet


Outlet Control - Submerged Inlet and Outlet
NOTE: See FHWA no. 5 for other possible conditions

| Figure 4.12 - Ditches Common Sections |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Properties of Ditches |  |  |  |  |  |  |  |  |
| NO. | Dimensions |  |  |  | Hydraulics |  |  |  |
|  | Side Slopes | B | H | W | A | WP | R | $\mathrm{R}^{(2 / 3)}$ |
| D-1 | -- | -- | 6.5 " | 5'-0" | 1.84 | 5.16 | 0.356 | 0.502 |
| D-1C | -- | -- | 6 " | 25'-0" | 6.25 | 25.50 | 0.245 | 0.392 |
| D-2A | 1.5:1 | 2'-0" | $1^{\prime}-0^{\prime \prime}$ | 5'-0" | 3.50 | 5.61 | 0.624 | 0.731 |
| B | 2:1 | 2'-0" | $1^{\prime}-0 \prime \prime$ | 6'-0" | 4.00 | 6.47 | 0.618 | 0.726 |
| C | 3:1 | 2'-0" | $1^{\prime}-0 \prime \prime$ | 8'-0" | 5.00 | 8.32 | 0.601 | 0.712 |
| D-3A | 1.5:1 | $3^{\prime}-0^{\prime \prime}$ | $1^{\prime}-6{ }^{\prime \prime}$ | 7'-6" | 7.88 | 8.41 | 0.937 | 0.957 |
| B | 2:1 | 3'-0" | 1'-6" | 9'-0" | 9.00 | 9.71 | 0.927 | 0.951 |
| C | 3:1 | $3^{\prime}-0^{\prime \prime}$ | $1^{\prime}-6^{\prime \prime}$ | 12'-0" | 11.25 | 12.49 | 0.901 | 0.933 |
| D-4A | 1.5:1 | $3^{\prime}-0^{\prime \prime}$ | 2'-0" | 9'-0" | 12.00 | 10.21 | 1.175 | 1.114 |
| B | 2:1 | $3^{\prime}-0^{\prime \prime}$ | $2^{\prime}-0^{\prime \prime}$ | 11'-0" | 14.00 | 11.94 | 1.172 | 1.112 |
| C | 3:1 | 3'-0" | 2'-0" | 15'-0" | 18.00 | 15.65 | 1.150 | 1.098 |
| D-5A | 1.5:1 | $4^{\prime}-0^{\prime \prime}$ | $3^{\prime}-0 \prime \prime$ | 13'-0" | 25.50 | 13.82 | 1.846 | 1.505 |
| B | 2:1 | $4^{\prime}-0^{\prime \prime}$ | $3^{\prime}-0 \prime \prime$ | 16'-0" | 30.00 | 16.42 | 1.827 | 1.495 |
| C | 3:1 | $4^{\prime}-0^{\prime \prime}$ | $3^{\prime}-0 \prime \prime$ | 22'-0" | 39.00 | 21.97 | 1.775 | 1.466 |
| D-6A | 2:1 | -- | $1^{\prime}-0^{\prime \prime}$ | 4'-0" | 2.00 | 4.47 | 0.447 | 0.585 |
| B | 3:1 | -- | $1^{\prime}-0 \prime \prime$ | 6'-0" | 3.00 | 6.32 | 0.474 | 0.608 |
| D-7A | 2:1 | -- | 2'-0" | 8'-0" | 8.00 | 8.94 | 0.894 | 0.928 |
| B | 3:1 | -- | 2'-0" | 12'-0" | 12.00 | 12.65 | 0.949 | 0.965 |
| D-8A | 2:1 | -- | $3^{\prime}-0^{\prime \prime}$ | 12'-0" | 18.00 | 13.42 | 1.342 | 1.216 |
| B | 3:1 | -- | 3'-0" | 18'-0" | 27.00 | 18.97 | 1.423 | 1.265 |
| D-9 | 7:1 | -- | $1^{\prime}-0 \prime \prime$ | 14'-0" | 7.00 | 14.14 | 0.495 | 0.626 |
| D-10 | 7:1 | -- | 2'-0" | 28'-0" | 28.00 | 28.28 | 0.990 | 0.993 |
| D-11 | 7:1 | -- | $3^{\prime}-0 \prime \prime$ | 42'-0" | 63.00 | 42.43 | 1.485 | 1.302 |



NOTE: A) Chart based on Manning formula $\mathrm{Q}=1.49 / \Pi^{*} \mathrm{~A} * \mathrm{R} 2 / 3 * \mathrm{~S} 1 / 2$ with $n=0.030$, except $D-1 C$ which is based on $n=0.015$. For other values of $n$, multiply discharge by 0.030 in


Example: Given- Slope $=3.3^{\prime}$ per 1000 ' discharge $=6.3$ c.f.s., $n=0.025$.
Required- Size of ditch and velocity. Solution- To use chart, multiply discharge, 6.3 by $(.03 / .025)=7.56 \mathrm{c} . f$.s. Point satisfying given conditions lies between lines for D-2A and D-2B. Select larger of the two ditches, in this case D-2B. Velocity approx. 2.1 ft . per sec.




| Section | Area A | Wetted perimeter P | Hydraulic radius R | Top width W | Hydraulic depth D | Section factor Z |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $-\infty$ <br> Rectangle$\square$ | by | $b+2 y$ | $\frac{b y}{b+2 y}$ | $b$ | $y$ | $b y^{1.5}$ |
| 4 | $(b+z y) y$ | $b+2 y \sqrt{1+z^{2}}$ | $\frac{(b+z y) y}{b+2 y \sqrt{1+z^{2}}}$ | $b+2 z y$ | $\frac{(b+z y) y}{b+2 z y}$ | $\frac{[(b+z y) y]^{1.5}}{\sqrt{b+2 z y}}$ |
| $\underbrace{-T}_{\text {Triagle }}$ | $z y^{2}$ | $2 y \sqrt{1+z^{2}}$ | $\frac{z y}{2 \sqrt{1+z^{2}}}$ | $2 z y$ | $1 / 2 y$ | $\frac{\sqrt{2}}{2} z y^{2.5}$ |
|  | ${ }^{1} / 8(\theta Đ \sin \theta) d_{0}^{2}$ | ${ }^{1 / 2} \theta d_{\hat{u}}$ | $1 / 4\left(1 \mathrm{D}_{\theta}^{\text {sin } \theta}\right) d \hat{u}$ | $\begin{aligned} & (\sin (1 / 2 \theta) d) \text { or } \\ & 2 \sqrt{y\left(d_{u} Ð y\right)} \end{aligned}$ | $1 / 8\left(\frac{\theta Đ \sin \theta}{\sin ^{1} / 2 \theta}\right) d_{\hat{u}}$ | $\frac{\sqrt{2}}{32} \frac{(\theta \boxplus \sin \theta)^{1.5}}{\left(\sin ^{1} / 2 \theta\right)^{0.5}} d_{\hat{u}}^{2.5}$ |
|  | 2/37y | $T+\frac{8 y^{2}}{3 T}{ }^{*}$ | ${\frac{2 T^{2} y}{3 T^{2}+8 y^{2}}}^{*}$ | $\frac{3 A}{2 y}$ | $2 / 3 y$ | $2 / 9 \sqrt{6} 7{ }^{1.5}$ |
|  | $\left(\frac{\ddagger}{2} \oplus 2\right) r^{2}+(b+2 r) y$ | $(\neq$ Đ 2 ) $r+b+2 y$ | $\frac{\left(\frac{( }{2} \mathrm{D} 2\right) r^{2}+(b+2 r) y}{(\neq \text { Đ } 2) r+b+2 y}$ | $b+2 r$ | $\frac{\left(\frac{\ddagger}{2} \oplus 2\right) r^{2}}{(b+2 r)}+y$ | $\frac{\left[\left(\frac{\#}{2} \oplus 2\right) r^{2}+(b+2 r) y\right]^{5}}{\sqrt{b+2 y}}$ |
|  | $\frac{T^{2}}{4 z}-\frac{r^{2}}{z}\left(1 Đ z \operatorname{cof}^{1} z\right)$ | $\frac{T}{z} \sqrt{1+z^{2}}-\frac{2 r}{z}\left(1 Đ z \operatorname{cof}^{1} z\right)$ | $\frac{A}{P}$ | $2[\mathrm{z}(y \mathrm{\square} \mathrm{r})+w \sqrt{1+z}]$ | $\frac{A}{T}$ | $A \sqrt{\frac{A}{T}}$ |
| *Satisfactory approximation for the interval $0<\mathrm{x}^{\prime \prime} 1$, where $\mathrm{x}=4 \mathrm{y} / \mathrm{T}$. When $\mathrm{x}>1$, use the exact expression $P=(\mathrm{T} / 2)\left[\sqrt{1+x^{2}}+1 / x \ln \left(x+\sqrt{1+x^{2}}\right)\right]$ |  |  |  |  |  |  |

Figure 4.15 - Flow Splitter, Option A


Note: The water quality discharge pipe may require an orifice plate to be installed on the outlet to control the height of the design water surface (weir height). The design water surface should be set to provide a minimum headwater/diameter ratio of 2.0 on the outlet pipe.

Figure 4.16 - Flow Splitter, Option B

*NOTE: Diameter (d) of standpipe should be large enough to minimize head above water quality design water surface and to keep water quality design flows from increasing more than $10 \%$ during 100 -year flows.

Figure 4.17 - Flow Spreader Option A: Anchored Plate

Example of anchored plate used with a sand filter* (may also be used with other water quality facilities).


PLAN VIEW
NTS


Alternative Design
Catch basin recommended for higher flow situations (generally for inflow velocities of 5 fps or greater for 100 year storm).

Figure 4.18 - Flow Spreader Option B: Concrete Sump Box

Example of a concrete sump flow spreader used with a biofiltration swale (may be used with other WQ facilities).


Note: Extend sides into slope. Height of side wall and wing walls must be sufficient to handle the 100-year flow or the highest flow entering the facility.

## SECTION A-A NTS



Figure 4.19 - Flow Spreader Option C: Notched Curb Spreader


FRONT VIEW A-A
NTS


Figure 4.20 - Flow Spreader Option D: Through-Curb Port


CURB PORT NTS

